

iber	iname	Area		
d				
ary				
	Cleaners	6.00 m²		
	Cleaners	6.00 m ²		
	Store	6.81 m ²		
iry: 3		18.81 m²		
ation				
	Corridor	41.81 m ²		
	Stairs	17.04 m ²		
	Corridor	31.44 m ²		
	Corridor	30.98 m ²		
	Stairs	14.55 m ²		
	Lift	5.65 m ²		
	Corridor	11.19 m ²		
ation:	7	152.66 m ²		
	nd Recention			
ice ai		$6.62 m^2$		
		4.95 m^2		
	Waiting	4.95 m^2		
	Recen/Security	16.13 m ²		
	Control Lobby	6.07 m^2		
	Vis WC	3 48 m ²		
	Search	6.64 m ²		
	Acc WC	6.73 m ²		
	Family Visit 1	15.00 m ²		
	Interview/Family Visit 2	15.00 m ²		
ice ar	nd Reception: 10	99 74 m ²		
		00.7 1 111		
	Diant	$16.02 m^2$		
		16.03 m ²		
	Switch	3.60 m^2		
Switch		1.50 11		
3		23.32 m²		
sion				
	Sec. Lounge 2	11.11 m ²		
	Seclusion 2	11.73 m ²		
	Seclusion Ensuite	4.57 m ²		
	Sec. Lounge 1	11.10 m ²		
	Seclusion 1	11.73 m ²		
	Seclusion Ensuite	4.57 m²		

017	Multi Faith Room	9.20 m²
018	Staff Base	16.27 m²
019	Servery Kitchen	15.30 m²
020	Dining Room	26.57 m²
021	Corridor	47.65 m²
022	Group Room	14.80 m²
023	Quiet Lounge	14.40 m ²
024	Assisted Bed	18.39 m²
025	Bed 9	15.01 m²
026	Dirty Util	10.00 m ²
027	Acc. WC	5.19 m²
028	WC	3.07 m²
029	Store	3.57 m²
030	Srv	0.73 m²
031	Bed 8	15.01 m²
032	Bed 7	15.01 m²
034	Bed 6	15.01 m²
035	Bed 5	15.21 m²
036	Srv	0.73 m²
037	Bed 4	14.96 m²
038	Patient Laundry	11.00 m ²
039	Corridor	55.46 m²
040	Staff Base	7.19 m²
041	Bed 3	14.59 m²
043	Bed 2	15.12 m²
044	Bed 1	15.22 m²
045	Srv	0.79 m²
046	Bed 11	15.01 m²
047	Srv	0.79 m²
048	Bed 10	15.01 m²
049	Asst. Bathroom	16.00 m²
051	Linen	5.79 m²
052	Ward Man.	14.45 m²
053	Ptnt Poss.	6.00 m²
120	Srv	0.73 m²
122	Corridor	16.24 m²
125	Store	7.30 m²
137	Srv	0.73 m²
/ard 1: 44		573.61 m²
/ard 2		
054	Air Lock	7.96 m²
055	Treatment Room	16.28 m²
056	Clinic with dispensary	7.43 m²

Number	Name	Area
0.062	Staff Base	16.38 m ²
0.063	Servery Kitchen	15.30 m ²
0.064	26.57 m ²	
0.065	Group Room	14.80 m ²
0.066	Quiet Lounge	14.40 m ²
0.67	Assisted Bed (12)	18.39 m ²
0.068	Bed 11	15.01 m ²
0.069	Dirty Util	10.00 m ²
0.070	Acc. WC	5.19 m ²
0.071	WC	3.07 m ²
0.072	Ptnt Poss.	6.00 m ²
0.073	Room	0.73 m²
0.074	Bed 10	15.01 m ²
0.075	Bed 9	15.01 m ²
0.076	Room	0.73 m ²
0.077	Bed 8	15.01 m ²
0.078	Bed 7	15.01 m ²
0.079	Room	0.73 m ²
0.080	Bed 6	15.01 m ²
0.081	Bed 5	15.21 m ²
0.082	Staff Base	7.19 m ²
0.083	Corridor	52.43 m ²
0.084	Patient Laundry	11.00 m ²
0.086	Bed 2	15.12 m ²
0.087	Bed 1	15.22 m ²
0.088	Srv	0.79 m²
0.089	Bed 4	14.96 m ²
0.090	Srv	0.79 m²
0.091	Bed 3	14.59 m ²
0.092	Asst. Bathroom	16.00 m ²
0.094	Linen	5.79 m²
0.095	Store	3.57 m ²
0.096	Ward Manager	14.45 m ²
0.121	Corridor	16.30 m ²
0.126	Store	7.30 m ²
0.138	Room	0.73 m²
Ward 2: 44		573.65 m²
Ground: 12	25	1628.93 m
First		
Ancillary		
,		

0.130
1.019
1.020
1.026
1.028
Circulation
Office
1.001
1.002
1.004
1.022
1.023
1.024
1.029
Office: 7

Ancillary		
1.005	Cleaners	7.22 m ²
1.025	Patient Poss. St.	8.52 m ²
Ancillary: 2		15.74 m²
Circulation		
0.129	Corridor	35.35 m ²

y: 7 al		110.67 m²
	Tribunal/MDT Room	21.66 m ²
al: 1		21.66 m ²
	Air Lock	7.96 m ²
	Treatment Room	16.28 m ²
	Clinic with disponsory	$7.42 m^2$

Air Lock	7.96 m ²
Treatment Room	16.28 m ²
Clinic with dispensary	7.43 m ²
Dispensing	5.83 m²
Interview	10.04 m ²

This drawing is copyright. Do not scale dimensions from this drawing "if in doubt ask". This drawing is to be read in conjunction with all other relevant drawings and specifications. All discrepancies on this drawing are to be reported to the architect. Do not modify any element of this drawing up only for purpose(s) issued.

		Designs referencing and based on:	P4 First Floor updated P5 Amendments to layout
edule of Accommo	odation	• WHBN 03-01 - Adult Acute Mental U	P6 Issue for Planning Pre-Applicatio
Name	Area	-	
T tainto	7104	 Environmental Design Guide: Adult M 	Aedium Secure
Corridor	$11.55 m^2$	Services - Department of Health	
Staire	10.60 m ²	-	
	5 65 m ²	 Best Practice Guideance - Specificat 	ion for adult
Stair	21 43 m ²	medium secure services - Departmer	nt of Health
Corridor	8 64 m ²	-	
6	102.21 m ²	 Standards for Forensic Mental Health and Medium Secure Care - Royal Co Psychiatrists 	I Services: Low llege of
Office	20.05 m ²		
Records Store	7.50 m ²	Confirmation from Priory that enric	aklar or similar
MDT Room	23.99 m ²	fire fighting equipment would be w	auirod for an
Meeting Room	15.00 m ²	future development on this site	equired for any
Consultant Office	10.00 m ²	inture development on this site	
Consultant Office	10.00 m ²		
Training Room	30.90 m ²	• Proposal looks to re-use as much	rootprint of the
	117.44 m²	recently razed Treowen building as achieving current space standards 2 x 12 bod wards	and visibility
Lobby	6.11 m ²		
Plant Room	62.54 m ²	-	
Tank Room	17.14 m ²	Comparison	
Server Room	12.92 m ²	Comparison	
	98.70 m ²	Existing Treowen areas:	
es		18 Beds	
F Staff Change/Loc	12.00 m ²		
F Staff Shwr	6.54 m ²	Ground Floor:	$1160m^{2}$
WC	3.13 m ²		240~2
Acc WC	5.49 m ²		
WC	3.13 m ²		1400m2
M Staff Shwr	6.54 m ²	Differences	0400
M Staff Change/Loc	12.00 m ²	Difference:	613m2
Staff Room	20.00 m ²		
es: 8	68.82 m²		_
	402.92 m²	Rooms causing significant increase	in area
	2031.85 m²	(inc associated circulation allowance	e):
		- 6 x bedrooms:	120m2
		- Duplication of Lounges, kitchen	230m2
		Dining room, Staff Offices, Clinic, visitor facilities	
		- Tribunal Suite:	80m2
			J J J



APPENDIX D – DEVELOPMENT ADVICE MAP





APPENDIX E – NATIONAL FLOOD RISK PLUVIAL FLOOD MAPS





Map Po Pluvial	erygl Llifogydd / Flood Risk Map - I Low Risk Extent
Allwed Flor	Id / Map Key od Risk Areas Cardiff Flintshire Gwynedd Coast Monmouthshire Newport North Wales Coast South Wales Coast South Wales Valleys Swansea Bay Wrexham face Water and Small Watercourses Extent + v Risk Low Extent



Map Pe Pluvial	erygl Llifogydd / Flood Risk Map - I Low Risk Hazard
Allwed	d / Map Key od Risk Areas
In the second se	Flintshire Gwynedd Coast Monmouthshire Newport North Wales Coast South Wales Coast South Wales Valleys Swansea Bay Wrexham face Water and Small Watercourses Hazard w Risk Low Danger for Some Danger for Most Danger for Most







APPENDIX F – NATIONAL FLOOD RISK FLUVIAL FLOOD MAPS













APPENDIX G – FLOOD ALERT MAP

tetratecheurope.com





APPENDIX H – DRAINAGE STRATEGY REPORT



Egerton House 2 Tower Road Birkenhead Wirral CH41 1FN



Priory Llanarth Court, Monmouthshire

Drainage Strategy Report

24/01/2020

Document Owner(s)	Project/Organization Role
Vince Williams	Civil Engineer

Project Report Control

Version	Date	Author	Change Description
P1		V Williams	Original Issue

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Ar 1.0 II 2.0 F 4.0 (SUS ⁻	opendix G - Surface Water Calculations 16 opendix H – Maintenance Strategy Report 23 NTRODUCTION 23 UTURE MAINTENANCE 23 COMPLIANCE WITH LASOO NON-STATUTORY TECHNICAL STANDARDS FOR FAINABLE DRAINAGE:BEST PRACTICE GUIDANCEERROR! BOOKMARK NOT DEFINED.

1.0 INTRODUCTION

Following a devastating accidental fire on 28th April 2020 which completely destroyed the existing secure mental hospital building, the Hospital Trust are proposing to reconstruct a new unit on the site OF the former unit, whilst updating the facilities to provide care for the residents.

2.0 COMPETENCY OF DESIGNER

MDA, Wirral LTD is a long established multi-discipline Consultancy, which provides design solutions for a range of site drainage and Flood Risk Assessments for developers in the UK. MDA liaise regularly with the Environment Agency, LLFA's and Water Authorities to ensure the designs comply with current statutory and regulatory requirements.

3.0 SITE LOCATION AND DESCRIPTION

The site is located 0.7km to the South-East of Llanarth Town Centre and 25km North-East of Newport Town Centre

The fire damaged building is located within the grounds of the Llanarth Court Hospital, made up of a number of existing hospital building's access, parking and landscaping. This report relates only to the re-development area within the wider site confines.

Following the devastating fire, the site has retained the original building foundation and floor slab with demolition rubble still present on site. An existing gravel path, macadam surfaced access road is still present with the remainder given over to grass.

Reference (NGR) for the approximate center of the site is 338242E, 210732N. The site location plan is included in Appendix A.

The total site development zone covers an area of approximately 0.644ha.

The sites boundaries are flanked by open fields east, existing hospital units to the west and woodland to the north and south

Historically the earliest map of 1881 show the main site as a stately home with the re-development area of the site as undeveloped farmland until it was developed between 1985 & 2004

The British Geological Society (BGS) maps indicate the site geology as:

- Superficial deposits of Alluvium Clay, Silt, Sand and Gravel
- Bedrock geology of St Maughans formation Argillaceous rocks and subequal/subordinate sandstone, interbedded
- The nearest BH log located approximately 1.6km to the SE indicates a mixture of sandstone and marl bands to a depth of 60m (end of BH). Water was struck at 5m level with the 'at rest' level 15m below ground level.
- A series of BH's relating to the A4 construction works 1.2km to the south indicate stiff sandy clays with some gravel and sandstone fragments to 3.5m depth.

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- Sandstone was present at 4.5m depth with overlying superficial deposits to the North East of the site, similarly sandy clays of 5m depth overlying sandstones, marl and mudstone to the North-West.
- In the absence of site borehole logs it is assessed that the site will have approx. 4m depth of sandy silty clays overlying bands of marl and sandstone to depth.

4.0 POTENTIAL FLOOD RISK

Natural Resources Wales flood map indicates the site lies within a Flood Zone B (area known to have previously flooded), however, looking at the detailed floor risk maps from rivers, surface water and small watercourses indicates only the surrounding area of the development is at risk of less than 150mm depth, whilst the actual development site shows no risk of flooding.

The Flood Risk Maps have been examined and are included in Appendix B.

5.0 EXISTING SITE DRAINAGE

The on-site drainage is classed as Private and thus maintained by the Hospital Trust's maintenance team.

The development site Foul Drainage network connected the building down the eastern and western sides before joining at the southern gable side of the building. The Foul Drainage then connects via a 150mm diameter pipe to the wider site drainage system to the east of the development boundary, with connections from the remaining on-site buildings prior to discharging to either of two storage tanks located to the South-West area of the wider site. The use of an air ram injector station then passes the site wide foul flows to the off-site Dwr Cymru / Welsh Water Treatment Works located to the north of the hospital site.

The roof drainage is collected on the north, east and west building façade before interconnecting at the south-west corner of the building before it outfalls in a southerly direction into a French drain located along the southern boundary of the site. This has been laid so it falls in both an easterly and westerly direction.

The drain exits at the eastern corner of the site via a piped system into a catchpit, which also connects an open ditch south of and outside of the site boundary limits. From the catchpit the outflow enters the Clawdd Brook flowing in a south-westerly direction.

The westerly exit point of the French drain is into an open ditch where it crosses under the track via a pipeline, exiting into an open ditch again connecting into the Clawdd Brook.

There are a number of additional outfalls from the wider site discharging into the Clawdd Brook, which opens into a wider 'pond' at the south-western edge of the wider site. This outflow from this pond is controlled by a weir gate, with the outflow continuing south-weterly until it discharges into the River Usk.

6.0 DRAINAGE COMPLIANCE STANDARDS

The development shall be in accordance with all current codes of practice and legislation. Hydraulic design of all sewers will be carried out using industry standard software Causeway Flow.

The Building Regulations - Approved Document H (2002) details a hierarchy of potential methods for disposing of surface water as shown below in order of preference:

- Discharge via infiltration
- Discharge to watercourse
- Discharge to sewer

Schedule 3 of the Flood and Water Management Act (FWMA) 2010 requires surface water drainage for new developments to comply with mandatory National Standards for sustainable drainage (SuDS).

Surface water drainage systems must be designed and built in accordance with these mandatory standards for sustainable drainage published by Welsh Ministers. These systems must be approved by the local authority acting in its Sustainable Drainage Systems (SuDS) Approving Body (SAB) role before construction work begins.

In line with Sewers for Adoption (7th Edition), the requirements for the design of a new surface water drainage systems are as follows:

- Below ground piped drainage to be sized to accommodate the 1 in 2-year (50% AEP) design storm without surcharge.
- System to be designed not to flood any part of the site in a 1 in 30-year (3% AEP) design storm.
- For events in exceedance of the 1 in 30-year design storm and up to and including the 1 in 100-year event, site drainage and topography should be designed where practicable to route surface water run-off away from buildings to safe above-ground storage areas on site, thereby preventing this run-off from leaving the site and increasing flood risk elsewhere.

For each design case described above, the design storm is the critical storm duration for the site conditions. For the 1 in 100-year design case, a 30% increase in the peak rainfall intensity is applied to allow for the estimated worst case impacts of climate change. This is in accordance with Table 5 of the Technical Guidance to the National Planning Policy Framework.

Suitable systems of below ground drainage will be required to contain as a minimum requirement, the 1 in 30-year event. Additionally, surface water run-off from events that exceed the design capacity of the new drainage system, up to and including the 1 in 100-year (+30%) event, will be retained on site to prevent any flood risk to the proposed development or any areas surrounding the site.

Therefore, the surface water drainage systems are to be designed to restrict the discharge to the required rate, up to and including a 1 in 100 year return period design storm (+30% climate change allowance).

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Foul water drainage disposal is set out in Part H of the Building Regulations in order of priority the preferred methods are:

- 1. Public sewer
- 2. Septic tank
- 3. Cesspool.

The foul water system shall be designed in accordance with;

- BS EN 752:2008 (Drain and sewer systems outside buildings)
- Sewers for Adoption (7th Edition)
- Technical Guidance to the National Planning Policy Framework document (Department for Communities and Local Government, March 2012)
- BS EN 12056-2:2000 (Drainage systems inside buildings)
- Building Regulations Approved Document H, Drainage and waste disposal. (Office of the Deputy Prime Minister, December 2010)

7.0 ASSESSMENT OF EXISTING AND PROPOSED RUN-OFF

As detailed in section 3.0 above, the existing site has a total area of 0.644Ha, of which the existing impermeable areas affected by the re-development zone have been measured as 1821m2 and the proposed impermeable areas being 2322m2. This will result in a 27% increase in impermeable areas.

The proposed surface water discharge rates will be assessed against the following conditions:

- 1 in 1-year storm event
- 1 in 30-year storm event
- 1 in 100-year storm event plus an allowance of 30% for climate change

8.0 DRAINAGE STRATEGY

The drainage networks have been designed to suit the proposed site layout and topography, with the aim to provide an effective and efficient design, mimicking the existing drainage as far as practicably possible

All site drainage will remain the responsibility of the Hospital Trust as it will form an extension of the current on-site drainage systems.

7.1 Surface Water

As indicated in Section 6, there is a requirement for the mandatory use of SUDS techniques. At present the BRE 365 percolation tests have yet to be completed and as such the drainage calculations have used generic permeability figures associated with sandy silty clays and will be adjusted at a later date to reflect the actual on-site results. Based on these results it is unlikely that effective infiltration solutions will be viable on their own in providing the design solutions.

Priory Llanarth Court, Monmouthshire

This is born-out by the existing site drainage utilizing the Brook for the outflow. The Hospital Trust's maintenance manager has further confirmed the site is generally wet hence the wider site containing numerous open water courses etc.

The nearest suitable water course within close proximity to the proposed development site is the Clawdd Brook located slightly to the south of the proposed site

The scheme is to be designed to achieve a discharge rate of no greater than 70% of the current brownfield site for the 2-year critical storm event, plus the greenfield run-off rate.

The current brownfield element for 2-year storm events have been calculated as 17.1 l/sec. Therefore, the surface water drainage systems are to be designed to restrict the discharge to the required rate of no more than (70% of 17.1) 12 l/sec, up to and including a 1 in 100 (+CC) return period design storm.

The intention is to collect the roof drainage and discharge this into a new attenuation pond located at the SW corner of the development area with a controlled outflow limiting the discharge rate to 12 l/sec maximum, with the outfall connected into the existing outfall into the existing French drain and thus to the existing brook. The outfall from the new pond will be set at a level that ensures the available free volume, from dry weather water level to the top of embankment, provides adequate storage capacity for all storm durations upto and including the 1:30 events. The proposed access road will be designed such that the surface water runs off to the south and east kerb channels where they will be directed to a new stone filter drain running alongside, this will remove the risk of any pollution entering the pond and affecting the likely eco system which it assumed will take advantage of the new pond habitat, whilst mimicking the existing site access drainage.

As the discharge rate will be less than the existing rates it is assessed that this will result in additional downstream storage being available providing additional on-site benefits with regards to future storm flooding events.

For the 1:100 storm duration events it has been calculated that an exceedance volume will result of circa 3m3 of on-site flooding. As the pond is located at the lowest part of the site with the ground levels generally falling away to the south any flood exceedance water will exit into the woods and thence onto the brook ensuring no on-site flooding of new or existing building can occur.

The same would apply should a catastrophic failure of the network occur, the flood route would be away from any buildings and to the south.

Storm event	Existing discharge rate (I/sec)	Proposed discharge rate (I/sec)
1:1	13.5	
1:2	17.1	
1:30	28.7	
1:100	33.7	

7.2 Foul Water

The intention for the development is to collect all of the required foul water discharge from the proposed development and discharge these via a gravity system to the on-site sewer which will remain a private system

It has been estimated that the original foul discharge rate would have been approximately 7.1 l/sec and the proposed development will generate approximately 7.3 l/sec. As such there is a very small increase in flow and is therefore assessed as not having any detrimental impact on the existing site drainage.

9.0 CONCLUSIONS

- The site is located within Flood Zone B, with a low probability of flooding.
- It is a legal requirement to utilise SuDS for all new schemes
- A suitable water course for direct discharge exists within the site which has an existing outfall which will be utilised where possible.
- The flow of surface water estimated from the proposed development is to be restricted to 12 l/sec, discharging to the on-site sewer after passing through a detention/percolation pond.
- Foul water drainage is required to serve the proposed development and will discharge to the on-site sewer network. As the estimated flow rate is only marginally greater than the existing rates it is determined that there is no requirement to approach the local water authority to obtain consent for this development.



Appendix A - Site Location Plan

Appendix B - Flood Map



Appendix C - Existing Site Layout







Appendix E - Drainage Layout Plan



Proposed

Appendix F - Surface Water Calculations

Existing Drainage

Aethodolog eriod (years inal Flow (% FSR Region Ratio-F Ct Entry (mins Name S1 C S2 S3 S4 C DUTFALL DS Node S2 S3 S3 OUTFALL Name View	y FSR) 2) 0 n Engle) 14.00 R 0.200 v 0.750) 5.00 Area 1 (ha) (0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (el Caj	and and Wa 20 20 20 20 20 20 20 5.00 36 36 36 36 36 36 36 36 36 36	Design: Ma ieles No swer Dian swel (m m) 3800 500 100 500 100 500 100 500 34.98 500 35.50 500 34.98 500 34.98	Settings eximum 1 Enfor des meter am) 1200 1 1200 1 10 3 10 3 10 3 10 3 10 3 10 3 10 3	Time of Con Maximum Minimu Minimu finimum Bad Preferred Include Inter rce best prac Easting (m) 338265.847 338276.778 338226.824 338216.053 338216.053 338216.022	Northing (m) 210767.2: 210705.4: 210705.4: 210705.4: 210705.4: 210705.9: Slope (1) (1:X) (n) 100.8 100.7 100.9	mins) 30.0 nyhr) 50.0 (m/s) 1.00 Type Leve t (m) 0.20 h (m) 1.20 ound \checkmark rules \checkmark 8 Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia T of (mm) (mins 150 5.8) 150 5.8)	0 (Soffits 0 0 0 (mm/hr) 5 32.6 3 31.1 3 32.7
Aethodologi eriod (years FSR Region MS-60 (m Ratio-F CV Entry (mins Name S1 0 51 0 52 53 54 0 DUTFALL DS Node S2 53 53 0 UTFALL Name Va	y FSR () 2 () 0 n Engla () 14.00 R 0.200 V 0.750 () 5.00 Area 7 (ha) () 0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (e) Cap	and and Wa 20 20 20 20 20 20 20 5.00 36 36 36 36 36 36 36 36 36 36	Ma les No per Dian m) 3800 500 100 100 100 100 100 100 1	M Enfor des meter mm) 1200 1 1200 1 100 100	Time of Conv Maximum Minimum Binimum Baci Preferred Include Inter rece best prace Easting (m) 338265.847 338226.824 338216.022 EL Fall n) (m) 985 0.515 467 0.518 009 0.491	Northing (m) 210767.2: 210705.4: 210705.4: 210705.4: 210705.4: 210705.9: Slope (1) (1:X) (n) 100.8	mins) 30.0 m/hr) 50.0 Type Leve t (m) 0.20 h (m) 1.20 ound \checkmark rules \checkmark g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia T of (mm) (mins) 150 5.8 150 5.8	C Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
eriod (years inal Flow (% FSR Region MS-60 (mm Ratio-f C) Entry (mins Name S1 C) S3 S4 C) DUTFALL DS Node S2 S3 OUTFALL Name Variation S3 S4 C) S3 S4 C) DUTFALL	() 2 () 2 () 0 n Engla () 14.00 R 0.200 V 0.750 () 5.00 Area 1 (ha) () 0.091 Lengt (m) 51.92 52.952 L 10.81 (e) Cap	and and Wa 00 0 7 of E Co (milns) Lo (5.00 36 36 5.00 37, 36 5.00 37, 36 th ks (mn n 22 0.6 13 0.6 13 0.6 13 0.6 13 0.6 14 0.6 15 0.6 16 0.6 16 0.6 17 0.6 18 0.6 19 0.6 10 0.6 19	No No No No No No No No No No	M Enfor meter am) 1200 : 1200 : 120 : 1200 :	Maximum Minimu Inimum Bad Preferred Include Inter rece best prace Easting (m) 338265.847 338277.778 338226.824 338216.053 338216.053 338216.053 338216.053 338216.053 338216.0515 467 0.515 467 0.515	Rainfall (mr m Velocity (Connection kdrop Heigh Cover Depti mediate Gm ttice design 210767.2/ 210716.7/ 210705.4/ 210705.9/ 210705.9/ 210705.9/ Slope ((1:X) (m 100.8 100.7 100.9	n/hr) 50.0 (m/s) 1.00 Type Leve t (m) 0.20 h (m) 1.20 ound \checkmark rules \checkmark g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia T of C nm) (mins 150 5.8 150 5.8	Sofflits 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Inal Flow (% FSR Region M5-60 (mm Ratio-f C) Entry (mins 100 C) Entry	 a) 0 m Engla i) 14.00 R 0.200 v 0.750 i) 5.00 Area 1 (ha) (i) 0.091 0.091	Tof E Co (mins) Lo 5.00 36 5.00 37, 36 5.00 36 5.00 37, 36 5.00 36 5.00 37, 36 5.00 36 5.00 36 5.00 37, 36 5.00 36 5.00 36 5.00 37, 36 5.00 36 5.00 36 5.00 36 5.00 37, 36 5.00 36 5.00 36 5.00 36 5.00 37, 36 5.00 36 5.00 37, 36 5.00 36 5.00 37 5.00 36 5.00 36 5.00 37 5.00 36 5.00 37 5.00 36 5.00 37 5.00 36 5.00 37 5.00 36 5.00 36 5.00 36 5.00 36 5.00 36 5.00 50 5.00 50	No No No No No No No No No No	M Enfor meter mm) 1200 : 1200 : 120 : 1200 :	Minimu Minimum Badi Preferred Include Inter rece best prace Easting (m) 338265.847 338226.824 338216.053 338216.022 IL Fall n) (m) 965 0.515 467 0.518 009 0.491	m Velocity (Connection kdrop Heigh Cover Depti mediate Gm titce design 210767.22 210716.7 210705.4 210705.9 210705.9 Slope ((1:X) (n 100.8 100.7 100.9	(m/s) 1.00 Type Leve t (m) 0.20 h (m) 1.20 ound √ rules √ g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.8 150 5.8	Sofflits 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Name Market Name Market Si C Si C Si C Si C Si C Si C Si C Si C	Area 1 (ha) 14.00 R 0.200 (ha) 5.00 Area 1 (ha) (i 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091	Tof E Co (mins) Lo (5.00 36 36 5.00 37, 36 th ks (mn n 22 0,6 13 0,6 13 0,6	No Sver Dian svel (m m) 1800 100 100 100 100 100 100 10	M Enfor meter mm) 1200 : 1200	(inimum Bad Preferred Include Inter rce best prace (m) 338265.847 338277.778 338226.824 338216.053 338216.053 338216.022 (IL Fall n) (m) 965 0.515 467 0.518 009 0.491	Cover Depti mediate Gn tice design 210767.22 210716.7 210705.4 210705.9 Slope ((1:X) (n 100.8 100.7 100.9	type beve t (m) 0.20 h (m) 1.20 ound √ rules √ g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.8 150 5.8	C Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
Ratio-F CV Entry (mins Name 51 C 32 33 34 C DUTFALL DS Node 52 53 53 OUTFALL Name Vi	R 0.200 V 0.750 (ha) (i 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091 0.091	T of E Co (mins) Lo (5.00 36 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 36 36 5.00 36 36 36 36 36 36 36 36 36 36 36 36 36 3	No ever Dian m) 1800 100 100 100 100 100 100 10	enformeter meter mm) 1200 1 1200 1 100 100	Preferred Include Inter rce best prace (m) 338265.847 338277.778 338226.824 338216.053 338216.053 338216.022 IL Fall n) (m) 865 0.515 467 0.518 009 0.491	Cover Depti mediate Gri ttice design 210767.2: 210716.7: 210705.4: 210705.9: Slope ((1:X) (n 100.8 100.7 100.9	h (m) 1.20 ound √ rules √ 8 Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 01a T of (nm) (mins 150 5.8 150 5.8	C Rain) (mm/hr) 5 32,6 3 31,1 3 32,7
Name A S1 C S2 S3 S4 C DUTFALL Name VA	V 0.750 i) 5.00 Area 1 (ha) (i) 0.091 0	T of E Co (mins) Lo (5.00 36 36 5.00 37 36 5.00 37 36 th ks (mn n 22 0.6 13 0.6	No ever Dian avel (m m) 3800 500 100 100 100 100 100 100 1	Information 1200 <td>Easting (m) 338265.847 338277.778 338226.824 338216.053 338216.022 EL Fall n) (m) 985 0.515 467 0.518 009 0.491</td> <td>Northing (m) 210767.2: 210716.7: 210705.4: 210705.9: 210705.9: 210705.9: 5lope (1) (1:X) (n) 100.8 100.7 100.9</td> <td>ound √ rules √ s Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.80 150 5.80</td> <td>Rain (mm/hr) 32,6 31,1 32,7 32,7</td>	Easting (m) 338265.847 338277.778 338226.824 338216.053 338216.022 EL Fall n) (m) 985 0.515 467 0.518 009 0.491	Northing (m) 210767.2: 210716.7: 210705.4: 210705.9: 210705.9: 210705.9: 5lope (1) (1:X) (n) 100.8 100.7 100.9	ound √ rules √ s Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.80 150 5.80	Rain (mm/hr) 32,6 31,1 32,7 32,7
Name / S1 0 S2 S3 S4 0 OUTFALL DS Node S2 S3 OUTFALL Name Vi	(ha) 5,00 Area 1 (ha) (0,091 0,091 0,091 Lengt (m) 51,92 52,18 49,52 L 10,81 (el Caj	Tof E Co mins) Lu (5.00 36 36 36 5.00 37 36 5.00 37 36 5.00 37 36 13 10 12 10 12 12 13 10 10 12 10 10 12 10 10 10 10 10 10 10 10 10 10 10 10 10	No wer Diam wel (m m) 1800 100	Enformeter meter meter 1200 1 1200	Easting (m) 338265.847 338277.778 338226.824 338216.053 338216.022 EL Fall n) (m) 985 0.515 467 0.518 009 0.491	Northing (m) 210767.2 210716.7 210705.4 210705.4 210705.9 Slope ((1:X) (n 100.8 100.7 100.9	rules √ g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.80 150 5.80	Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
Name /	Area 1 (ha) (r 0.091 0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (el Caj	Tof E Co (mins) Lo 36 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 37 36 5.00 36 36 5.00 37 36 36 36 5.00 37 36 36 36 36 36 36 36 36 36 36 36 36 36	No over m) (3000 Dian (m) (m) (m) (m) (3000 (m) (5000 (1000 (m) (7000 (m) (1000 (m)	des meter am) 1200 1 1200 1 1 1200 1 1 1200 1 1 1200 1 1 1200 1 1 1200 1 1 1200 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Easting (m) 3382265.847 3382277.778 338226.824 338216.053 338216.022 IIL Fall n) (m) 965 0.515 467 0.518 009 0.491	Northing (m) 210767.21 210716.71 210705.41 210705.91 210705.91 210705.91 210705.91 210705.91 (1:X) (n 100.8 100.7 100.9	g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof C nm) (mins 150 5.81 150 5.81	Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
Name //	Area 7 (ha) (r 0.091 0.091 0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (el Caj	Tof E Co (mins) Lo (5.00 36 36 5.00 37 36 5.00 37 36 th ks (mm n 22 0.6 13 0.6	over Dian avel (m asso (m asso (m asso (m asso (m) (m) (m) (m) (m) boold (m) (m) (m) 600 35.50 600 34.98 600 34.46	meter am) 1200 1 1200 1 1 100 1 100 100	Easting (m) 338265.847 338277.778 338226.824 338216.053 338216.053 338216.022 EL Fall n) (m) 985 0.515 467 0.518 009 0.491	Northing (m) 210767.21 210705.41 210705.91 210005.91 21005.91 21005.91 21005.91 21005.91 21005.91 21005.91	g Depth (m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia Tof (mm) (mins 150 5.80 150 5.80	Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
51 C 52 53 54 C DUTFALL DS Node 52 53 S3 OUTFALL Name Va	(ha) (r 0.091 0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (el Caj	mins) Lo (1) 5.00 36 36 36 36 36 36 36 36 36 36 36 36 36 3	avel (m m) (800 (500 (700 (700 (700 (700 (700 (700 (7	am) 1200 : 1200 : 1	(m) 338265.847 338277.778 338226.824 338216.053 338216.022 ill Fall n) (m) 985 0.515 467 0.518 009 0.491	(m) 210767.2: 210716.7: 210705.4: 210705.9: 210705.9: (1:X) (n) 100.8 100.7 100.9	(m) 89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 01a T of C nm) (mins 150 5.81 150 5.81 150 5.83	C Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
51 0 52 53 54 0 DUTFALL DS Node 52 53 S3 OUTFALL Name Va	0.091 0.091 Lengt (m) 51.92 52.18 49.52 L 10.81 (e) Cap	5.00 36 36 5.00 37 36 th ks (mn n 22 0.0 13 0.0	(300 (500 (700 (100 (700 (700 (700 (700) (100 (700) (1	1200 1 1200 1	338265.847 338277.778 338226.824 338216.053 338216.022	210767.2/ 210716.7/ 210705.4/ 210705.9/ 210705.9/ Slope ((1:X) (n 100.8 100.7 100.9	89 1.300 56 1.515 72 2.233 08 1.600 56 2.341 Dia T of C nma) (mins) 150 5.8 150 5.8 150 5.8	Rain (mm/hr) 32,6 31,1 32,7 32,7
32 53 54 C DUTFALL DS Node 52 53 53 OUTFALL Name Vi	Lengt (m) 51.92 52.18 49.52 L 10.81	36 36 5,00 37 36 th ks (mn n 22 0,6 13 0,6 13 0,6	.100 .100 .700 Lin n)/ US II (m) 500 35.50 500 34.98 600 35.50 500 34.46	1200 1 1200 1 11	338277.778 338226.824 338216.053 338216.022 IL Fall n) (m) 985 0.515 467 0.518 009 0.491	210716.7 210705.4 210753.8 210705.9 Slope ((1:X) (n 100.8 100.7 100.9	56 1.515 72 2.233 08 1.600 56 2.341 01a T of (mm) (mins 150 5.80 150 6.73	Rain (mm/hr) 32,6 31,1 32,7 32,7
DUTFALL DS Node S2 S3 S3 OUTFALL Name	Lengt (m) 51.92 52.18 49.52 L 10.81	36 5,00 37 36 th ks (mn 22 0,6 13 0,6 13 0,6	100 100 100 100 100 100 100 100	1200 1 1200 1 100 100	338226.824 338216.053 338216.022 IL Fall n) (m) 985 0.515 467 0.518 009 0.491	210705.4 210753.8 210705.9 Slope ((1:X) (n 100.8 100.7 100.9	72 2.233 08 1.600 56 2.341 Dia Tof (nm) (mins 150 5.80 150 5.80	Rain (mm/hr) 32,6 31,1 32,7 32,7
DUTFALL DS Node S2 S3 S3 OUTFALL Name	Lengt (m) 51.92 52.18 49.52 L 10.81	stor 37 36 th ks (mn 22 0.6 13 0.6 13 0.6	100 100 100 100 100 100 100 100	1200 1 1200 1 1200 1 1200 1 1200 1 (m 00 34.9 15 34.4 10 35.0 17 34.3	338216.023 338216.022 ill Fall n) (m) 385 0.515 467 0.518 309 0.491	Slope ((1:X) (n 100.8 100.7 100.9	Dia Tof C nm) (mins 150 5.80 150 6.73 150 5.80	Rain) (mm/hr) 5 32.6 3 31.1 3 32.7
DS Node S2 S3 S3 OUTFALL	Lengt (m) 51.92 52.18 49.52 L 10.81	th ks (mn 12 0.0 18 0.0 13 0.0	Lin n) / US III (m) 500 35.50 500 34.98 500 35.50 500 34.45	nks L DS (m 0 34.9 35 34.4 0 35.0 7 34.3	ill. Fall n) (m) 985 0.515 467 0.518 009 0.491	Slope ((1:X) (n 100.8 100.7 100.9	Dia Tof (nm) (mins 150 5.8 150 6.7 150 5.8	Rain) (mm/hr) 6 32.6 3 31.1 3 32.7
DS Node S2 S3 OUTFALL Name	Lengt (m) 51.92 52.18 49.52 L 10.81	th ks (mn n 22 0.4 18 0.4 13 0.4	n)/ US II (m) 600 35.50 600 34.98 600 35.50 600 34.46	L DS (m 00 34.9 85 34.4 00 35.0 57 34.3	ilL Fall n) (m) 985 0.515 467 0.518 009 0.491	Slope ((1:X) (n 100.8 100.7 100.9	Dia Tof (nm) (mins 150 5.8 150 6.7 150 5.8	Rain (mm/hr) 32.6 31.1 32.7
Node S2 S3 S3 OUTFALL	(m) 51.92 52.18 49.52 L 10.81	8 22 0.6 18 0.6 13 0.6	(m) 500 35.50 500 34.98 500 35.50 500 34.45	(m 0 34.9 15 34.4 10 35.0 17 34.3	n) (m) 985 0.515 467 0.518 009 0.491	(1:X) (n 100.8 100.7 100.9	nm) (mins 150 5.80 150 6.73 150 5.80) (mm/hr) 5 32.6 3 31.1 3 32.7
S2 S3 OUTFALL	51.92 52.18 49.52 L 10.81	22 0.6 18 0.6 12 0.6 13 0.6	600 35.50 600 34.98 600 35.50 600 34.46	0 34.9 5 34.4 0 35.0 57 34.3	985 0.515 467 0.518 009 0.491	100.8 100.7 100.9	150 5.80 150 6.73 150 5.83	5 32.6 3 31.1 3 32.7
S3 S3 OUTFALL	52.18 49.52 L 10.81	ss 0.6 12 0.6 13 0.6	600 34.98 600 35.50 600 34.46	x 34.4 x 35.0 7 34.3	467 0.518 009 0.491	100.9	150 6.73 150 5.83	3 31.1 3 32.7
OUTFALL	L 10.81	13 0.6	600 34.46	7 34.3	003 0.431	100.9	190 9765	3 32.7
Name Vi	el Caj	n Daw			359 0.108	100.1	150 6.93	1 30.8
1		PROW	US	DS E	Ares EA	dd Pro	Pro	
(m)	/s) (l/s	s) (I/s)	Depth D	epth	(ha) Inflo	w Depth	Velocity	
			(m) ((m)	(1/1	s) (mm)	(m/s)	
51.0 1.0	00 17.	7 7.7	1365 2	083	0.091 0	10 /1	0.954	
S2.0 1.0	00 17.	7 8.1	1.450 1	.541	0.091 0	0.0 71	0.978	
51.2 1.0	004 17.	7 15.2	2.083 2	2.191	0.182 0	0.0 107	1.126	
			Pipeline	Schedul	le .			
ngth Slop	e Dia	Link	US CL	USIL	US Depth	DS CL	DS IL D	S Depth
.922 100	.8 15	0 Circular	36.800	35.500	1.150	36.500	34.985	1.365
.188 100.	7 15	0 Circular	36.500	34.985	1.365	36.700	34.467	2.083
.522 100.	.9 150	0 Circular	37.100	35.500	1.450	36.700	35.009	1.541
.813 100.	.1 150	0 Circular	35.700	34,467	2.083	36.700	34.359	2.191
k US	Dia	Node	MH	D	S Dia	Node	мн	
Node	(mm)	Түре	Түре	No	de (mm)	Туре	Туре	
1 52	1200	Manhole	Adoptable	53	1200	Manhole	Adoptable	e
.0 S4	1200	Manhole	Adoptable	\$3	1200	Manhole	Adoptable	c
	1200	Manhole	Adoptable	OUT	FALL 1200	Manhole	Adoptable	e
n le la	Slop n) (1:) 922 100 188 100 522 100 813 100 k US Node 0 0 \$1 1 \$2 0 \$4 2 \$3	Slope Dia m) (1:X) (mm) 922 100.8 15 188 100.7 15 522 100.9 15 813 100.1 15 k US Dia Node (mm) 0 0 S1 1200 1 52 1200 0 S4 1200 2 S3 1200	Slope Dia Link m) (1:X) (mm) Type 922 100.8 150 Circula 188 100.7 150 Circula 522 100.9 150 Circula 813 100.1 150 Circula k US Dia Node Node (mm) Type 0 S1 1200 Manhole 1 S2 1200 Manhole 2 S3 1200 Manhole	Slope Dia Link US CL m) (1:X) (mm) Type (m) 922 100.8 150 Circular 36.800 188 100.7 150 Circular 36.800 188 100.7 150 Circular 36.500 522 100.9 150 Circular 36.700 813 100.1 150 Circular 36.700 k US Dia Node MH Node (mm) Type Type Type 0 S1 1200 Manhole Adoptable 1 S2 1200 Manhole Adoptable 0 S4 1200 Manhole Adoptable 2 S3 1200 Manhole Adoptable	Slope Dia Link US CL US IL m) (1:X) (mm) Type (m) (m) 922 100.8 150 Circular 36.800 35.500 188 100.7 150 Circular 36.500 34.983 522 100.9 150 Circular 37.100 35.500 813 100.1 150 Circular 35.700 34.467 k US Dia Node MH D Node (mm) Type Type Ne 0 S1 1200 Manhole Adoptable S2 1 S2 1200 Manhole Adoptable S3 0 S4 1200 Manhole Adoptable S3 2 S3 1200 Manhole Adoptable OUT	Slope Dia Link US CL US IL US Depth m) (1:X) (mm) Type (m) (m) (m) 922 100.8 150 Circular 36.800 35.500 1.150 188 100.7 150 Circular 36.500 34.985 1.365 522 100.9 150 Circular 37.100 35.500 1.450 813 100.1 150 Circular 36.700 34.467 2.083 k US Dia Node MH DS Dia Node (mm) Type Type Node (mm) 0 S1 1200 Manhole Adoptable S2 1200 0 S4 1200 Manhole Adoptable S3 1200 2 S3 1200 Manhole Adoptable S3 1200	Slope Dia Link US CL US IL US Depth DS CL m) (1:X) (mm) Type (m) (m) (m) (m) (m) 922 100.8 150 Circular 36.500 35.500 1.150 36.500 188 100.7 150 Circular 36.500 34.985 1.365 36.700 522 100.9 150 Circular 36.700 34.467 2.083 36.700 813 100.1 150 Circular 36.700 34.467 2.083 36.700 k US Dia Node MH DS Dia Node Node (mm) Type Type Node (mm) Type 0 S1 1200 Manhole Adoptable S2 1200 Manhole 1 S2 1200 Manhole Adoptable S3 1200 Manhole 0 S4 1200	slope Dia Link US CL US IL US Depth DS CL DS IL D n) (1:X) (mm) Type (m) (m)



AUSEWAY 😳	/IDA Wirral Lt	d		File: EXX Network Stuart N 20/01/2	STING SW C Storm M loss 021	/ CALCULAT Network	IIO Page	4
Result	ts for 2 year (critical Sto	rm Durat	tion. Los	vest mas	s balance:	99.54%	
Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status
15 minute winte	None S1	(mins)	(m) 25.578	0.078	(1/5)	0 1965	0.0000	OF
15 minute winte	52	11	35.060	0.075	9.0	0.1903	0.0000	OK
15 minute winte	53	12	34.602	0.135	17.7	0.1530	0.0000	OK
15 minute winte	r \$4	11	35.576	0.076	9.2	0.1726	0.0000	OK
15 minute winte	OUTFALL	12	34.480	0.121	17.1	0.0000	0.0000	ОК
Link Event	US Link	DS	Outfl	ow Ve	locity F	low/Cap	Link	Discharge
(Outflow)	Node	Node	(1/s) (r	n/s)		Vol (m ³)	Vol (m ³)
15 minute winter	S1 S1.0	S2	144	9.0	1.027	0.508	0.4624	
15 minute winter	S2 S1.1	\$3		8.8	0.691	0.498	0.6597	
15 minute winter	S3 S1.2	OUTFAL	L 1	7.1	1.092	0.965	0.1726	8.5
15 minute winter	S4 S2.0	\$3		8.8	0.998	0.501	0,4393	
13 millione wither	54 52.0				0.000	0.001	0.4335	

	Resu					20/01,	2021				
		AS IOF	l year C	critical Sto	rm Dura	tion. L	owest mas	s balance:	99.54%		
	Node Event	,	US lode	Peak (mins)	Level (m)	Dept (m)	h Inflow (I√s)	Node Vol (m³)	Flood (m³)	Status	
	15 minute winte	er S1		10	35.567	0.06	7 7.2	0.1702	0.0000	OK	
	15 minute winte	er S2		11	35.050	0.06	5 7.0	0.0730	0.0000	OK	
	15 minute winte	er \$3		12	34.573	0.10	6 13.7	0.1199	0.0000	OK	
	15 minute winte	er S4		11	35.566	0.06	6 7.2	0.1493	0.0000	OK	
1	15 minute winte	er OL	ITFALL	12	34.456	0.09	7 13.5	0.0000	0.0000	OK	
	Link Event	US	Link	DS	Outf	low \	elocity F	low/Cap	Link	Discharge	
45	(Outriow)	Node	C1 0	Node	(W	5	(m/s)	0 200	VOI (m')	Vol (m-)	
10 1	minute winter	51	51.0	52		6.0	0.909	0.398	0.5041		
15 1	ninute winter	52	51.1	25 OUTEAU		0.0	1.001	0.367	0.5339		
15 r	ninute winter	53 54	\$2.0	S3		6.9	0.937	0.390	0.1375	0.0	

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AUSEWAT		rai Lto			Netw Stuar 20/01	ork: Storn t Moss 1/2021	W CALCUL/ Network	ATTO Pa	Si o
Resu	ts for 100	year (critica	al Storm	Duration.	Lowest r	nass balanc	o: 99.54	<u>%</u>
Node Event	US Node	Pe (m	eak ins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m ²)	Status
30 minute summer	S1	1	20	35,883	0.383	20.9	0.9685	0.0000	SURCHARGED
30 minute summer	S2		20	35,431	0.446	18.7	0.5039	0.0000	SURCHARGED
30 minute summer	\$3		20	34.997	0.530	33.7	0.5989	0.0000	SURCHARGED
30 minute summer	S4		19	35.688	0.188	20.9	0.4270	0.0000	SURCHARGED
15 minute summer	OUTFAL	L	10	34.501	0.142	32.5	0.0000	0.0000	OK
Link Fuent	us	Link		ns d	Dutflow	Velocity	Elow/Can	Link	Discharge
(Outflow)	Node	LIIIA	N	ode	(1/e)	(m/s)	riow/cap	Volta	³ Vol(m ²)
30 minute summer	S1	\$1.0	\$2	oue	18.7	1 169	1.057	0.91	41
30 minute summer	52	S1 1	62		16.2	0.919	0.014	0.91	88
30 minute summer	52	\$1.1	00	TEALL	22.7	1 016	1 001	0.51	\$4 36.4
30 minute summer	50	62.0	62	THE	10.0	1.146	1.074	0.10	20.4
so minute summer	34	52.0	33		19.0	1.140	1.0/4	0.82	02

CAUSEWAY 😜	MUAW	nrrai Lt	a		Stua 20/0	vork: Storr nt Moss 1/2021	n Network	AllO Pa	8e 2
Rest	alts for 30) year	Critical	Storm	Duration.	Lowest n	nass balance	e: 99.54%	i.
Node Event	US Nod	e (Peak mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m²)	Flood (m ³)	Status
15 minute winter	S1		10	35.61	0.119	17.0	0.3011	0.0000	OK
15 minute winter	S2		12	35.19	0.209	16.9	0.2367	0.0000	SURCHARGED
15 minute winter	\$3		11	34.863	0.396	29.7	0.4475	0.0000	SURCHARGED
15 minute winter	S4		11	35.61	0.117	17.0	0.2647	0.0000	OK
15 minute summer	OUTFA	ALL	12	34.50	0.142	28.1	0.0000	0.0000	ОК
Link Event (Outflow)	US Node	Link	D	de de	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m	Discharge Vol (m ²)
15 minute winter	S1	S1.0	S2		16.9	1.151	0.954	0.817	9
15 minute winter	\$2	S1.1	\$3		14.8	0.848	0.835	0.918	8
15 minute winter	\$3	S1.2	OUT	FALL	28.7	1.633	1.620	0.188	4 15.7
15 minute winter	S4	\$2.0	\$3		16.3	1.126	0.921	0.716	4

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Proposed Drainage

Appendix G – Maintenance Strategy Report

1.0 INTRODUCTION

This maintenance strategy report has been prepared in connection with a planning application for the redevelopment of a secure mental health unit at the existing Priory Llanarth Court hospital to provide state-of-theart care for residents and is to be read in conjunction with all manufacturer's recommendations and the Drainage Strategy Report

2.0 FUTURE MAINTENANCE

The proposed drainage solution uses SUDS techniques in accordance with the CIRIA SUDS Manual C753. The surface water run-off is restricted using a flow control device and the attenuated run-off stored using a detention pond, positioned upstream of the flow control.

The Surface water system within the development has been designed to accommodate upto the 30 year storm events as part of an on-line attenuation system, with the discharge being controlled utilising a flow control system, excess flows during a 100 year event will surcharge and overflow south into the wooded area, into the existing ditches and onto the Brook.

It is proposed that the plot drainage and attenuation pond will remain private at present.

The maintenance of the private systems as specified within this report will be detailed within the developments Operation and Maintenance Manual (O&M) which will be transferred to the Hospital Trust and form part of the inspection, maintenance and repair regime by their in-house maintenance team. The wider hospital site already has a number of open water courses and a large pond and as such the Hospital's maintenance team are familiar with the ongoing maintenance requirements associated with the proposed detention pond.

During the construction phase and defects liability period pre-handover of properties; the contractor, or his maintenance contractor, will be responsible for ensuring the ongoing inspection, maintenance and repairs of any drainage and SuDS systems as a minimum requirement identified within the report.

The works as detailed below are detailed in accordance with the CIRIA SuDS Manual C753 as per the operation and maintenance table 21.3 (modified) where relevant with additional information provided for systems not covered within the SuDS manual.

Maintenance Schedule	Required Action	Typical Frequency
	Remove litter and debris	Monthly
	Cut grass – meadow grass in and around ba	Half yearly (spring – before nesting season, and autumn)
Regular Maintenance	Manage other vegetation and remove nuisance plants	Monthly (at start,then as required)
	Inspect inlets, outlets and overflows for blockages, and clear if required	Monthly
	Inspect bank sides, structures, pipework etc for evidence of physical damage	Monthly

Table 21.3 (modified) : Operation and maintenance requirements for

Priory Llanarth Court, Monmouthshire

	Remove sediment from inlets and outlet	Annually or as required
Remedial Action	Repair erosion or other damage by reseeding or re-turfing	As required
Monitoring	Inspect / check all inletsand outlets ensure they are in good condition and operating as designed	Annually

The attenuation system has been provided with catchpit chambers The flow controller is to be maintained by the Hospital Trust's existing maintenance team.